High Speed Blade Screening

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Introduction

Whether you are designing blades for propellers or airfoils for high speed executive jets, as an engineer you must have an efficient tool that is capable of screening and designing custom airfoil shapes over all speeds of operations. An aerodynamic problem that arises (and this is a potential show stopper) is the tendency of the pressure drag to increase by an order of magnitude through the transonic regime of operation. This sudden drag rise depends on such factors as airfoil thickness, camber and angle of attack. For a propeller design, the efficiency can decrease dramatically after reaching a certain helical tip mach number (this limits forward airplane speed and/or available power). For a wing design, the performance of the airplane can be severely limited due to airfoil shapes that were poorly designed and tested across the transonic regime of flight. Engineers can avoid these problems by using VisualFoil Plus, our new software for airfoil analysis.

VisualFoil Plus is an update to version 4.1 that incorporates the capability to analyze airfoils at transonic and supersonic flows. Figure 1 shows the pressure drag rise for a NACA 2412 airfoil as predicted using VisualFoil Plus. The NACA 2412 is a popular airfoil for the wings of general aviation aircraft. It is also used in some propeller designs. Currently, propeller companies design and test propeller blades based on modern (often proprietary) airfoil shapes. Using an airfoil that pushes the drag rise towards the right side of the graph could result in a significant performance boost.

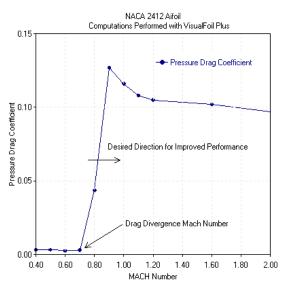
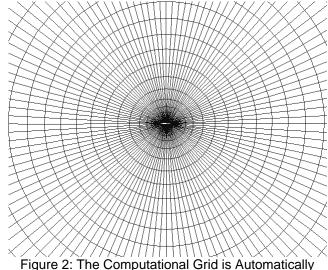


Figure 1: Pressure Drag as a function Mach Number.

VisualFoil Plus to the Rescue

VisualFoil Plus is the perfect screening tool for high speed airfoils. The program is easy-to-use, fast, accurate and has the capability to solve custom airfoils in addition to any of the over 1000 thousand airfoils in its built-in library. Airfoils can also be modified to a more efficient shape using the built-in airfoil modification tools.

The figures below show the detailed solution generated for producing figure 1. A typical run for the Euler solver is about one minute on a Pentium based notebook computer.



Generated So there is No Need for an External Grid Generation Package.

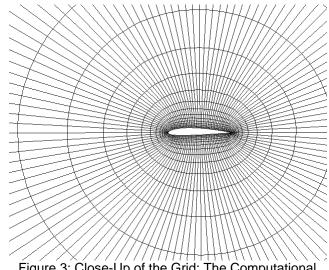


Figure 3: Close-Up of the Grid: The Computational Grid is Generated in less than a second for any of the thousands of airfoil found in VisualFoil Plus.

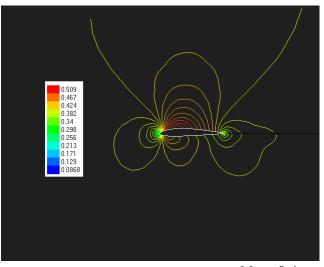


Figure 4: Mach Number Contours for $M_{_\infty}=0.4$

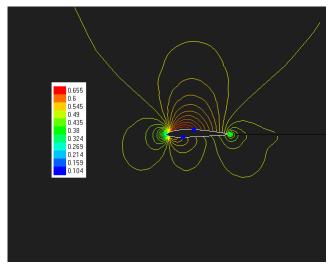
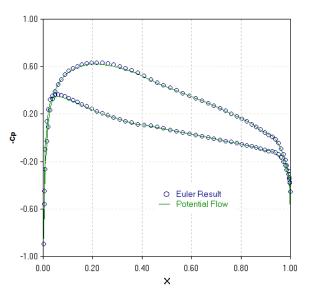


Figure 6: Mach Number Contours for $M_{_\infty}=0.5$



Pressure Coefficient (M=0.4)

Figure 5: Comparison of Potential & Compressible Solutions at M= 0.40. Note the similarity to the potential flow solution (modified with the Prandtl-Glauert correction factor).

Pressure Coefficient (M=0.5)

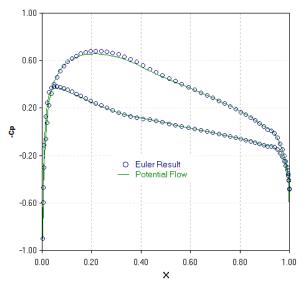


Figure 7: Comparison of Potential & Compressible Solutions at M= 0.50

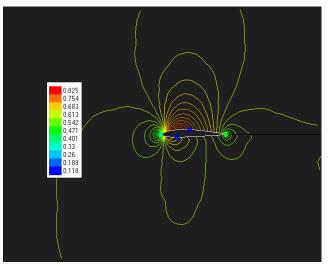


Figure 8: Mach Number Contours for $M_{_\infty} = 0.6$

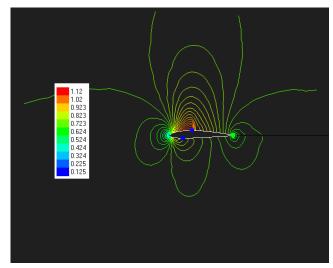


Figure 10: Mach Number Contours for $M_{\infty}=0.7$

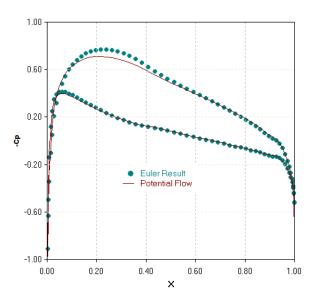


Figure 9: Comparison of Potential & Compressible Solutions at M= 0.60 . The compressible Flow solution begins to diverge from the Potential solution.

Pressure Coefficient (M=0.6)

Pressure Coefficient (M=0.7)

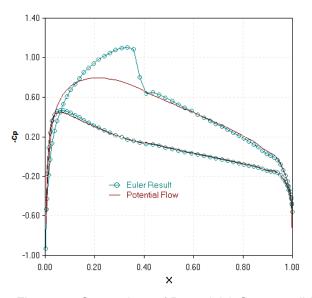


Figure 11: Comparison of Potential & Compressible Solutions at M= 0.70. The figure shows a divergence in the pressure coefficient from the potential solution at the upper surface of the airfoil.

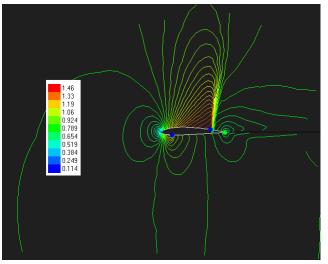


Figure 12: Mach Number Contours for $M_{\infty}=0.8$

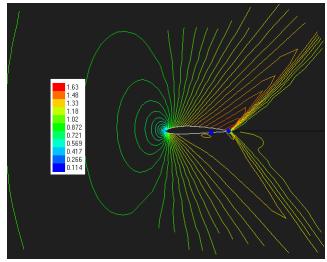
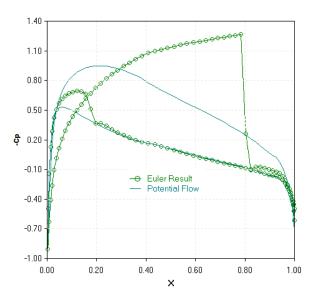


Figure 14: Mach Number Contours for $M_{\infty}=1.0$



Pressure Coefficient (M=0.8)

Figure 13: At M=0.8, the compressible pressure coefficient is radically different than the potential theory results on both the upper and lower surfaces of the airfoil.

Pressure Coefficient (M=1.0)

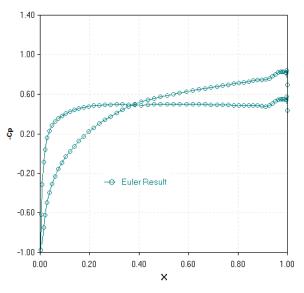


Figure 15: Subsonic Potential theory software can no longer predict the pressure coefficient at M=1.0.

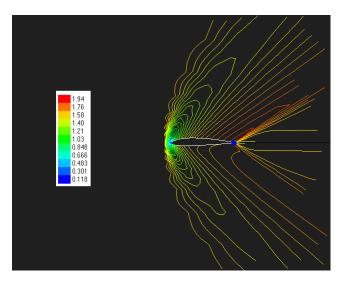
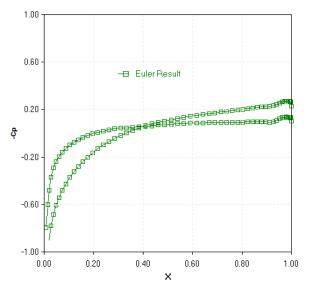


Figure 16: Mach Number Contours for $M_{\infty} = 1.6$



Pressure Coefficient (M=1.6)

Figure 17: Pressure Coefficient at M=1.6

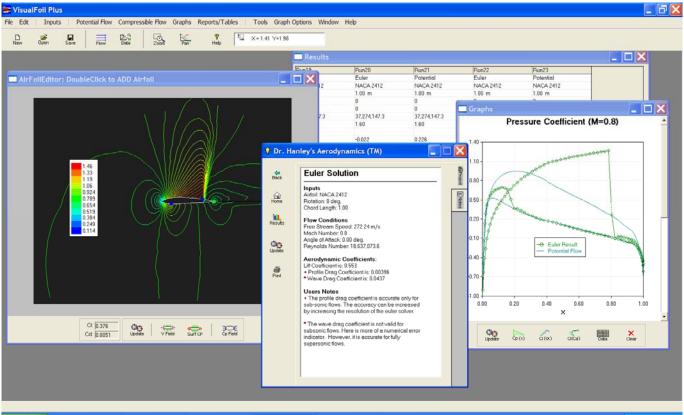
More Information

More information about VisualFoil Plus can be found at <u>http://www.hanleyinnovations.com</u>.

Screen Shots VisualFoil Plus _ 7 🗙 File Edit Inputs Potential Flow Compressible Flow Graphs Reports/Tables Tools Graph Options Window Help ♥ III ×=-2.32 Y=1.62 New Open Save How Data Zoom Pan Results - 🗆 🗙 AirFoilEditor: DoubleClick to ADD Airfoil Bun1 Bun2 Bun3 Run4 Bun5 Euler NACA 2412 1 00 m Euler NACA 2412 1.00 m Euler NACA 2412 Euler NACA 2412 Solution Type Potential NACA 2412 arfoil 1.00 m 1.00 m Chord 1.00 m AOA (Deg.) Rotation (Deg.) Reynolds No. Graphs _ 🗆 🗙 18,637,073.6 16,592,684.1 Pressure Coefficient (M=0.6) Mach No. 8.0 2.00 Coefficient 😯 Dr. Hanley's Aerodynamics (TM) 1.00 -Contraction of the same 0.754 Euler Solution Back 0.60 0.613 0.542 0.471 0.401 0.33 0.26 Inputs Airfoil: NACA 2412 Home Rotation 0 deg. Chord Length: 1.00 0.20 Flow Conditions Free Stream Speed: 204.18 m/s Mach Number: 0.6 Angle of Attack: 0.00 deg. Reynolds Number: 13,977,805.2 ******* al. 8 -0.20 90 Euler Result Potential Flow Aerodynamic Coefficients: Lift Coefficient is: 0.328 • Profile Drag Coefficient is: 0.00512 • Wave Drag Coefficient is: 0.00258 -0.60 Users Notes • The profile drag coefficient is accurate only for sub-sonic flows. The accuracy can be increased by increasing the resolution of the euler solver. -1.00 -0.00 0.20 0.40 0.60 0.80 1.00 × CI: 0.282 Cd: 0.00522 The wave drag coefficient is not valid for subsonic flows. Here is more of a numerical error indicator. However, it is accurate for fully supersonic flows. Update V Field Surf CP Cp Field 00 CI(Cd) Data Clear Geo (00)

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